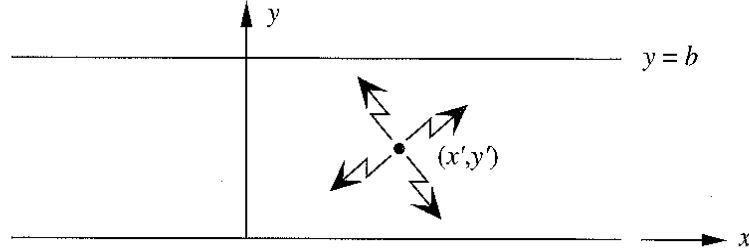


Two-Dimensional Green's Function

Consider the parallel plate waveguide excited by a line source at (x', y') :



We are interested in finding the Green's function of this configuration subject to the boundary conditions $G = 0$ at $y = 0, b$ and the radiation conditions at $x \rightarrow \pm\infty$.

We have

$$\frac{\partial^2 G}{\partial x^2} + \frac{\partial^2 G}{\partial y^2} + \beta_0^2 G = -\delta(x - x') \delta(y - y'), \quad \beta_0 = k_0 = \omega_0 \sqrt{\mu\epsilon}$$

and we propose the solution (by invoking separation of variables)

$$G = G_x G_y = G_x(x, x') G_y(y, y')$$

As done for the one-dimensional case we may choose (this sum is most appropriate for G_y since ψ_n will be sinusoidal and not decaying exponentials)

$$G_y = \sum_{n=-\infty}^{\infty} a_n \psi_n(y)$$

with

$$\psi_n''(y) + \beta_n^2 \psi_n(y) = 0, \quad \psi_n = 0 \text{ at } y = 0, b$$

It follows that

$$\psi_n(y) = A \sin \frac{n\pi}{b} y = \sqrt{\frac{2}{b}} \sin \frac{n\pi}{b} y \quad \text{with } \beta_n = \frac{n\pi}{b}$$

Note that $\psi_n(y)$ are the eigenfunctions and β_n are the associated eigenvalues of the problem.

We have chosen A so that

$$\int_0^b \psi(y) \psi_m(y) dy = \delta_{nm} = \begin{cases} 1 & n = m \\ 0 & n \neq m \end{cases}$$

i.e., ψ_n are orthonormal eigenfunctions.

Then

$$G = \sqrt{\frac{2}{b}} \sum_n a_n G_x(x, x') \sin \frac{n\pi}{b} y = \sum_n a_n \psi_n(y) G_x(x, x')$$

Substituting this into the D.E. satisfied by G gives

$$\sum_n a_n [G_x'' \psi_n + G_x \psi_n'' + \beta_0^2 G_x \psi_n] = -\delta(x - x') \delta(y - y')$$

Next we multiply both sides by ψ_m and integrate with respect to y to get (this step eliminates $\delta(y - y')$ and the y dependence)

$$a_m[G_x'' + (\beta_0^2 - \beta_m^2)G_x] = -\delta(x - x') \psi_m(y')$$

This leads to

$$\tilde{G}_x'' + (\beta_0^2 - \beta_n^2)\tilde{G}_x = -\delta(x - x')$$

where

$$\tilde{G}_x = G_x \underbrace{\frac{a_n}{\psi_n(y')}}_{\text{constant}}$$

Clearly, we have now reduced the 2D problem down to a corresponding 1D problem.

The solution of this latter D.E. was already given earlier and we have (since only the radiation condition need be satisfied)

$$\tilde{G}_x = \begin{cases} \frac{e^{-j\beta_{gn}x} e^{+j\beta_{gn}x'}}{2j\beta_{gn}} & x > x' \\ \frac{e^{-j\beta_{gn}x'} e^{+j\beta_{gn}x}}{2j\beta_{gn}} & x < x' \end{cases} = \frac{e^{-j\beta_{gn}|x-x'|}}{2j\beta_{gn}}$$

with

$$\beta_{gn} = \begin{cases} \sqrt{\beta_0^2 - \beta_n^2} & \beta_0 > \beta_n, \\ -j\sqrt{\beta_n^2 - \beta_0^2} & \beta_0 < \beta_n \end{cases} \quad \beta_0 = k_0 = \omega_0 \sqrt{\mu_0 \epsilon_0}$$

Returning back to G , we now have

$$\begin{aligned} G &= G_x G_y = \sum_n a_n \psi_n(y) G_x = \sum_n a_n \psi_n(y) \left[\frac{\psi_n(y')}{a_n} \right] \tilde{G}_x \\ &\Rightarrow G = \sum_n \psi_n(y) \psi_n(y') \frac{e^{-j\beta_{gn}|x-x'|}}{2j\beta_{gn}} \\ &\boxed{G = \frac{2}{b} \sum_n \sin \frac{n\pi}{b} y \sin \frac{n\pi}{b} y' \frac{e^{-j\beta_{gn}|x-x'|}}{2j\beta_{gn}}} \end{aligned}$$

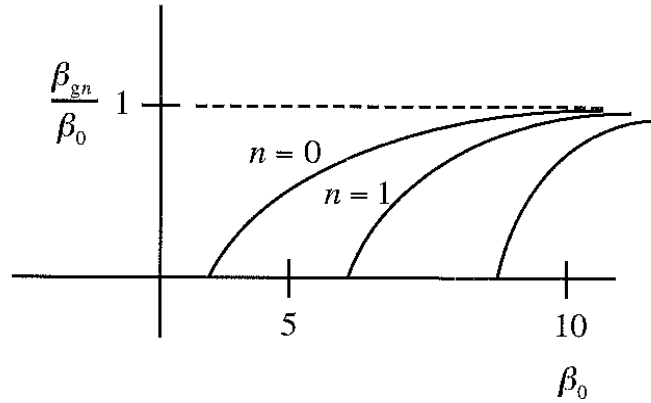
when $\beta_0 = 0$ (static case), it follows that

$$G = \sum_n \frac{1}{n\pi} \sin \frac{n\pi}{b} y \sin \frac{n\pi}{b} y' e^{-\beta_n |x-x'|}$$

and as expected G decays in the direction of $\pm x$, since there is no propagation at DC.

Each of the summands in the expression for G corresponds to a mode. The specific modal functions or eigenfunctions are given by

$$\phi_n(x, y) = C \sin \frac{n\pi}{b} y e^{\pm j\beta_{gn}x}, \quad C \text{ is a constant}$$



These modes propagate in the $\pm x$ direction, and since $\phi_n = 0$ at $y = 0, b$ (on the PEC surfaces), they can represent the electric field component E_z (TE wave) or E_x (TM). The mode phase velocity is

$$v_{np} = \frac{\omega}{\beta_{gn}} = \frac{v_{0p}}{\sqrt{1 - \left(\frac{n\pi}{\beta_0 b}\right)^2}} = \frac{c_0}{N \sqrt{1 - \left(\frac{n\pi}{\beta_0 b}\right)^2}} > v_{0p}$$

in which c_0 is the speed of light. Note that v_{np} is mode dependent and frequency dependent (i.e., the waveguide is dispersive). Also,

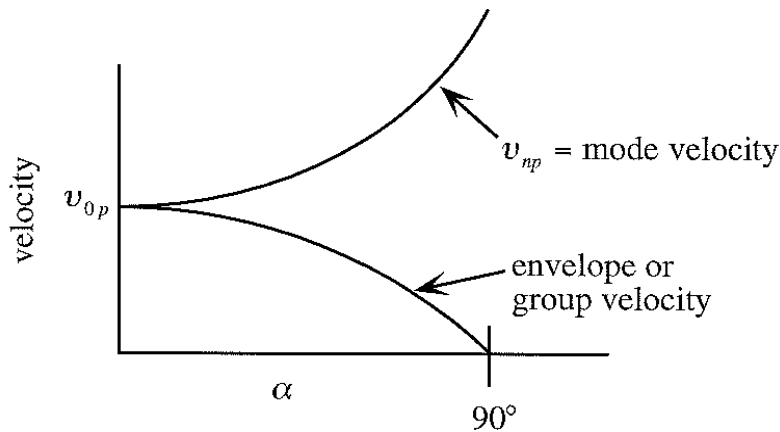
$$v_{0p}|_{n=0} = \frac{\omega}{\beta_{g0}} = \frac{\omega}{\beta_0} = \frac{1}{\sqrt{\mu\epsilon}} = \frac{c_0}{N}$$

If we define

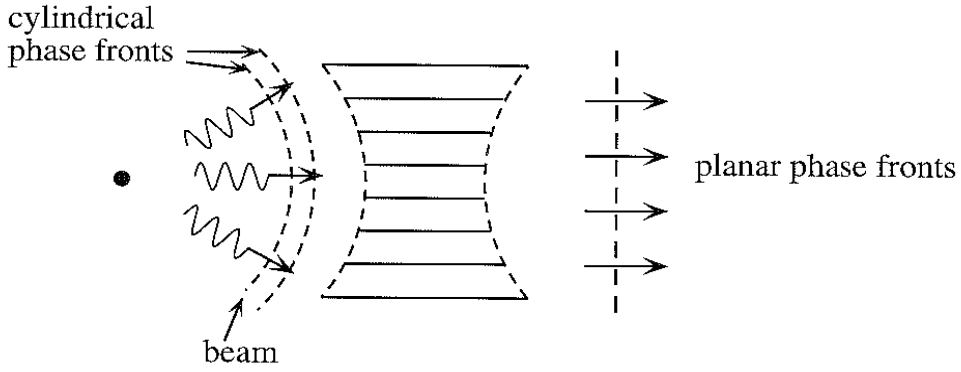
$$N_{eq} = N \sqrt{1 - \left(\frac{n\pi}{\beta_0 b}\right)^2} \quad \Rightarrow \quad v_{np} = \frac{c_0}{N_{eq}}$$

and we observe that

$$N_{eq} \leq N$$



This is the basis for designing microwave lenses.



Because the phase velocity in each guide formed by a pair of plates is greater than v_{0p} for a propagating mode (say TE_1), a cylindrical wave (or a beam) may exit as a plane wave on the right side.

Whether a mode propagates or attenuates as it travels along the x direction, this depends on the value of the propagation constant

$$\beta_{gn} = \begin{cases} \sqrt{\beta_0^2 - \beta_n^2} & \beta_0 > \beta_n \\ -j\sqrt{\beta_n^2 - \beta_0^2} & \beta_0 < \beta_n \end{cases}$$

For $\beta_0 > \beta_n$ the propagation factor is

$$e^{\pm j\sqrt{\beta_0^2 - \beta_n^2}x} \quad (\text{no attenuation})$$

and for $\beta_n > \beta_0$ we have

$$e^{-\sqrt{\beta_n^2 - \beta_0^2}|x|} \quad (\text{attenuating})$$

The transition from a propagating to an attenuating mode occurs when

$$\begin{aligned} \sqrt{\beta_0^2 - \beta_n^2} &= 0 & \omega_{0c}^2 \mu \epsilon &= \left(\frac{n\pi}{b}\right)^2 \implies \\ \omega_{0c} &= \frac{1}{\sqrt{\mu \epsilon}} \left(\frac{n\pi}{b}\right) = 2\pi f_{0c} \implies \\ f_{0c} &= \frac{n}{2b\sqrt{\mu \epsilon}} = \text{cutoff frequency for the } n\text{th mode} \end{aligned}$$

That is, if the excitation frequency is below f_{0c} ($f < f_{0c}$) the n th mode will not propagate. The associated cutoff wavelength is

$$\lambda_{0c} = \frac{v_{0p}}{f_{0c}} = \frac{1}{\sqrt{\mu \epsilon} f_{0c}} = \frac{2b}{n}$$

The wavelength of the mode in the guide is

$$\lambda_g = \frac{2\pi}{\beta_{gn}} = \frac{2\pi}{\beta_0 \sqrt{1 - \left(\frac{\omega_{0c}}{\omega_0}\right)^2}} = \frac{\lambda_0}{\sqrt{1 - \left(\frac{\lambda_0}{\lambda_{0c}}\right)^2}}$$

$$\boxed{\lambda_0 = \frac{v_{0p}}{f_0} = \frac{2\pi v_{0p}}{\omega_0}}$$

Group velocity

Each mode in the guide can be rewritten as

$$C \left(\frac{e^{j(n\pi/b)y} + e^{-j(n\pi/b)y}}{2j} \right) e^{\pm j\beta_{gn}x}$$

This constitutes the superposition of two plane waves ϕ_n^+ and ϕ_n^- , where

$$\phi_n^{\pm} = e^{-j[\beta_{gn}x \pm (n\pi/b)y]} \quad \beta_{gn} = \sqrt{\beta_0^2 - \left(\frac{n\pi}{b}\right)^2}$$

Recalling the typical plane wave expression

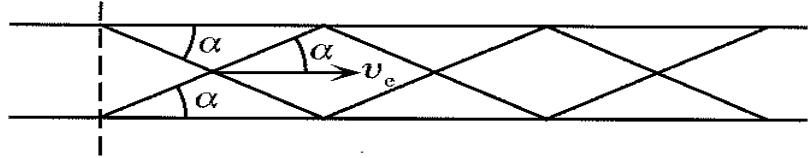
$$\phi \sim e^{-j\beta_0(x \cos \phi \pm y \sin \phi)}$$

we introduce the substitutions

$$\frac{n\pi}{b} = \beta_0 \sin \alpha \quad \Rightarrow \quad \beta_{gn} = \sqrt{\beta_0^2 - \beta_0^2 \sin^2 \alpha} = \beta_0 \cos \alpha$$

Thus

$$\phi_n^{\pm} = e^{-j\beta_0(x \cos \alpha \pm y \sin \alpha)}$$



The energy or group velocity for this mode/wave is given by

$$v_e = v_{0p} \cos \alpha = \underbrace{\left(\frac{c_0}{N}\right)}_{v_{0p}} \underbrace{\left(\frac{\beta_{gn}}{\beta_0}\right)}_{\cos \alpha} = \frac{c_0}{N} \sqrt{1 - \left(\frac{n\pi}{\beta_0 b}\right)^2} \leq v_{0p}$$

which is also a function of the excitation frequency. Note that in general

$$v_e = \frac{d\omega_0}{d\beta_g} = \frac{1}{\left(\frac{d\beta_g}{d\omega_0}\right)}$$

where β_g or β_{gn} is the propagation constant of the guided wave. Since

$$\begin{aligned} \frac{d\beta_g}{d\omega_0} &= \frac{d}{d\omega_0} \left(\sqrt{\beta_0^2 - \left(\frac{n\pi}{b}\right)^2} \right) = \frac{d}{d\omega_0} \left(\sqrt{\omega_0^2 \mu \epsilon - \left(\frac{n\pi}{b}\right)^2} \right) \\ &= \frac{\omega_0 \mu \epsilon}{\sqrt{\omega_0^2 \mu \epsilon - \left(\frac{n\pi}{b}\right)^2}} \\ &= \frac{N}{c_0} \frac{1}{\sqrt{1 - \left(\frac{n\pi}{\beta_0 b}\right)^2}} = \frac{1}{v_e} \end{aligned}$$

This expression agrees with the above, which was derived geometrically.

If $N = \sqrt{\mu_r \epsilon_r}$ is also a function of ω (material dispersion), then (note $\omega_0^2 \mu \epsilon = \beta_0^2$ and $\mu \epsilon = N^2 / c_0^2$)

$$\begin{aligned}
 \frac{d\beta_g}{d\omega_0} &= \frac{d}{d\omega_0} \left(\sqrt{\beta_0^2 - \frac{n\pi}{b}} \right) = \frac{d}{d\omega_0} \left(\sqrt{\omega_0^2 \mu \epsilon - \left(\frac{n\pi}{b} \right)^2} \right) \\
 &= \frac{\beta_0^2 c_0^2}{N^2} \frac{1}{2} \frac{d}{d\omega_0} (\omega_0^2 \mu \epsilon) \left[\sqrt{\quad} \right]^{-1} = \frac{1}{2} \frac{(d/d\omega_0)(\omega_0^2 \mu \epsilon)}{\sqrt{\omega_0^2 \mu \epsilon - \left(\frac{n\pi}{b} \right)^2}} \\
 \frac{d}{d\omega_0} (\omega_0^2 \mu \epsilon) &= 2\omega_0 \mu \epsilon + \frac{2\omega_0^2}{c_0^2} \frac{dN}{d\omega_0} \\
 &= 2\omega_0 \mu \epsilon + \frac{2\beta_0^2 c_0^2}{N^2 c_0^2} \frac{dN}{d\omega_0} = 2\omega_0 \mu \epsilon + \frac{2\beta_0^2}{N^2} \frac{dN}{d\omega_0}
 \end{aligned}$$

Thus,

$$\frac{d\beta_g}{d\omega_0} = \left(\frac{N}{c_0} + \frac{\omega_0}{c_0} \frac{dN}{d\omega_0} \right) \frac{1}{\sqrt{1 - \left(\frac{n\pi}{\beta_0 b} \right)^2}} = \frac{N}{c_0} \left(1 + \frac{\beta_0 c_0}{N^2} \frac{dN}{d\omega_0} \right) \frac{1}{\sqrt{1 - \left(\frac{n\pi}{\beta_0 b} \right)^2}}$$

and

$$\tilde{v}_e = \frac{1}{d\beta_g/d\omega_0} = \frac{c_0}{N} \left(1 - \frac{\omega_0}{N} \frac{dN}{d\omega_0} \right) \frac{1}{\sqrt{1 - \left(\frac{n\pi}{\beta_0 b} \right)^2}} = v_e \left(1 - \frac{\omega_0}{N} \frac{dN}{d\omega_0} \right)$$