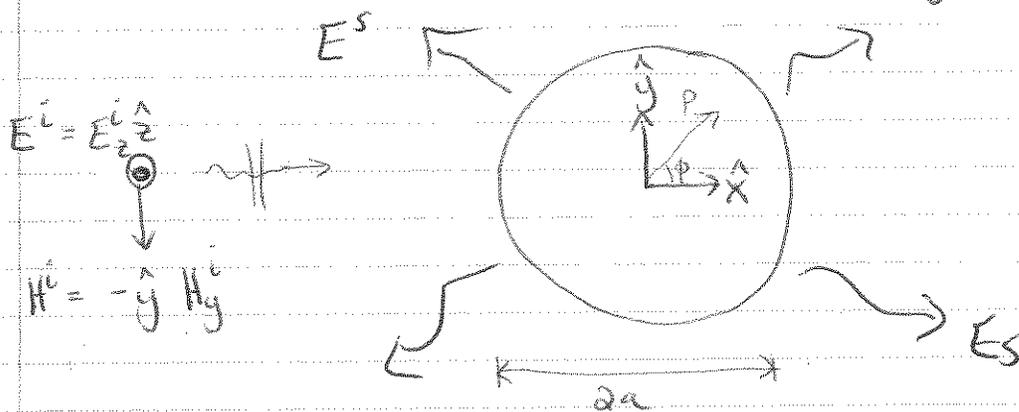


Scattering From an ^{infinite} PEC Cylinder ① (Balanis 11.5) pp. 607-617)

In order to characterize the interaction of a plane wave with a cylindrical object, we can represent the plane wave as a sum of cylindrical waves.

Note that this is possible because both plane waves & cylindrical waves form a "complete set" of modes. Thus any fields may be written as either a series of plane waves or as a series of cylindrical waves.

For TM_z incidence: (\vec{E} field along axis of cylinder)



$$\vec{E}^i = \hat{z} E_z^i = \hat{z} E_0 e^{-j\beta x} = \hat{z} E_0 e^{-j\beta \rho \cos \phi}$$

$$\vec{E}^i = \hat{z} E_0 \sum_{n=-\infty}^{\infty} j^{-n} J_n(\beta \rho) e^{jn\phi} \quad \left(\text{Balanis } 11-81a \right)$$

Note that $J_n(\beta \rho)$ is small for $\beta \rho \gg n$

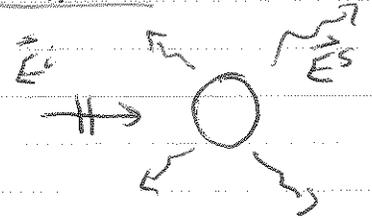
Thus # of required modes is proportional to electrical size (radius) of cylinder

For very small cylinders ($\beta a \rightarrow 0$), we only need $n=0$ term

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We can also represent the total field as the sum of the incident field plus the scattered field.

$$\vec{E}^t(p, \phi) = \vec{E}^i(p, \phi) + \vec{E}^s(p, \phi)$$



The scattered field can also be written as the sum of cylindrical waves:

$$\vec{E}^s = \hat{z} E_0 \sum_{n=-\infty}^{\infty} c_n \underbrace{H_n^{(2)}(\beta p)}_{\rightarrow \text{scattered fields are outward traveling}} e^{jn\phi}$$

where c_n is the coefficient of each Hankel fn (note: our c_n differs from that in Balanis)

Hankel functions are defined by the Bessel fns of 1st kind and are traveling waves

$$H_n^{(1)}(\beta p) = J_n(\beta p) + jY_n(\beta p) \quad \left(\begin{array}{l} \text{inward } (-\beta p) \\ \text{traveling wave} \end{array} \right)$$

$$H_n^{(2)}(\beta p) = J_n(\beta p) - jY_n(\beta p) \quad \left(\begin{array}{l} \text{outward } (+\beta p) \\ \text{traveling wave} \end{array} \right)$$

This is exactly analogous to:

$$e^{+j\beta x} = \cos(\beta x) + j \sin(\beta x) \quad \left(\begin{array}{l} \text{left } (-x) \text{ traveling} \\ \text{wave} \end{array} \right)$$

$$e^{-j\beta x} = \cos(\beta x) - j \sin(\beta x) \quad \left(\begin{array}{l} \text{right } (+x) \text{ traveling} \\ \text{wave} \end{array} \right)$$

Also note that the Bessel & Hankel fns. are only valid solutions of M.E. in source free regions when multiplied by appropriate angular variation, i.e. $e^{jn\phi}$ for 2D problems.

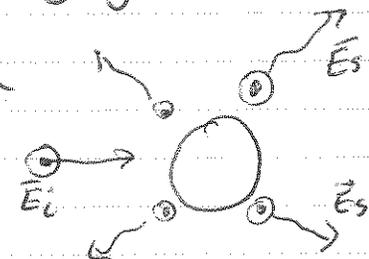
$$\Rightarrow J_n(\beta\rho)e^{jn\phi}, Y_n(\beta\rho)e^{jn\phi}$$

$$H_n^{(1)}(\beta\rho)e^{jn\phi}, H_n^{(2)}(\beta\rho)e^{jn\phi}$$

We solve for scattered fields by applying B.C.s

On PEC cylinder, $E_{tan}^t = 0 \big|_{\rho=a}$

$$\Rightarrow \boxed{E_z^i(\rho=a) + E_z^s(\rho=a) = 0}$$



$$\Rightarrow E_0 \sum_{n=-\infty}^{\infty} j^{-n} J_n(\beta a) e^{jn\phi} + E_0 \sum_{n=-\infty}^{\infty} c_n H_n^{(2)}(\beta a) e^{jn\phi} = 0$$

Since $e^{jn\phi}$ are orthogonal in $\phi \in [0, 2\pi)$ each n term must vanish independently

$$\Rightarrow j^{-n} J_n(\beta a) + c_n H_n^{(2)}(\beta a) = 0$$

$$\Rightarrow \boxed{c_n = -j^{-n} \frac{J_n(\beta a)}{H_n^{(2)}(\beta a)}}$$

(4)

We can therefore write the scattered E-field:

$$\vec{E}_s = -E_0 \hat{z} \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n(\beta a)}{H_n^{(2)}(\beta a)} H_n^{(2)}(\beta \rho) e^{jn\phi} \quad (\text{TM}_z \text{ incidence})$$

What do the scattered fields look like far away from the cylinder? (Far Fields)

The Hankel functions have an asymptotic approximation for $\beta \rho \rightarrow \infty$

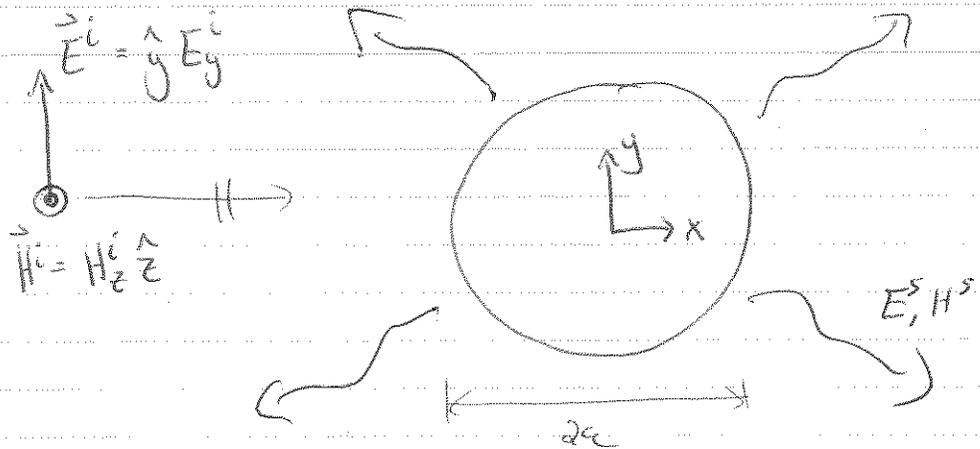
$$H_n^{(2)}(\beta \rho \rightarrow \text{large}) \approx \sqrt{\frac{2j}{\pi \beta \rho}} j^n e^{-j\beta \rho}$$

Note, this is an exponential traveling wave outwards ($+j\rho$) decaying as $1/\sqrt{\rho}$, which is a cylindrical wave.

$$\Rightarrow \vec{E}_s^{\text{FF}}(\beta \rho \rightarrow \text{large}) \approx -\hat{z} E_0 \sqrt{\frac{2j}{\pi \beta}} \frac{e^{-j\beta \rho}}{\sqrt{\rho}} \sum_{n=-\infty}^{\infty} \frac{J_n(\beta a)}{H_n^{(2)}(\beta a)} j^n e^{jn\phi}$$

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Scattering from a PEC cylinder, TE_z incidence
(\vec{H} field along axis of cylinder)



Expand incident plane wave as cylindrical series:

$$\vec{H}^i = \hat{z} H_0 e^{-j\beta x} = \hat{z} H_0 \sum_{n=-\infty}^{\infty} j^{-n} J_n(\beta \rho) e^{jn\phi}$$

We must calculate \vec{E}^i since the PEC BC. require us to evaluate E field

$$\vec{E}^i = \frac{1}{j\omega\epsilon} \nabla \times \vec{H}^i = \frac{1}{j\omega\epsilon} \left(\hat{\rho} \frac{1}{\rho} \frac{\partial H_z^i}{\partial \phi} - \hat{\phi} \frac{\partial H_z^i}{\partial \rho} \right) \quad (\text{Balanis p. 956})$$

$$E_{\rho}^i = \frac{H_0}{j\omega\epsilon} \left(\frac{1}{\rho} \sum_{n=-\infty}^{\infty} (jn) j^{-n} J_n(\beta \rho) e^{jn\phi} \right)$$

$$E_{\phi}^i = \frac{-H_0}{j\omega\epsilon} \left(\sum_{n=-\infty}^{\infty} j^{-n} \frac{\partial J_n(\beta \rho)}{\partial \beta \rho} \cdot \beta e^{jn\phi} \right)$$

Write this as $J_n'(\beta \rho)$, note there are simple recursive def. of Bessel fn. derivatives

(6)

Similarly, we write the scattered field as:

$$\vec{H}^s = \hat{z} H_0 \sum_{n=-\infty}^{\infty} d_n H_n^{(2)}(\beta \rho) e^{jn\phi}$$

$$E_\rho^s = \frac{1}{j\omega\epsilon} \frac{1}{\rho} \frac{\partial H_z^s}{\partial \phi} = \frac{H_0}{\omega\epsilon} \frac{1}{\rho} \sum_{n=-\infty}^{\infty} d_n n H_n^{(2)}(\beta \rho) e^{jn\phi}$$

$$E_\phi^s = -\frac{\beta H_0}{j\omega\epsilon} \sum_{n=-\infty}^{\infty} d_n H_n^{(2)'}(\beta \rho) e^{jn\phi}$$

Enforce BC.: $E_{tan}^t(\rho=a) = 0$

$$E_\phi^i(\rho=a) + E_\phi^s(\rho=a) = 0$$

$$-\frac{H_0 \beta}{j\omega\epsilon} \sum_{n=-\infty}^{\infty} j^{-n} J_n'(\beta a) e^{jn\phi} - \frac{H_0 \beta}{j\omega\epsilon} \sum_{n=-\infty}^{\infty} d_n H_n^{(2)'}(\beta a) e^{jn\phi} = 0$$

again, individual n terms must $\rightarrow 0$

$$j^{-n} J_n'(\beta a) + d_n H_n^{(2)'}(\beta a) = 0$$

$$d_n = -j^{-n} \frac{J_n'(\beta a)}{H_n^{(2)'}(\beta a)}$$

$$\vec{H}^s = -\hat{z} H_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n'(\beta a)}{H_n^{(2)'}(\beta a)} H_n^{(2)}(\beta \rho) e^{jn\phi}$$

(TE_z incidence)