

Determination of the Mode Coefficients

Consider a waveguide structure whose infinite dimension is along the z direction. Defining the TE and TM eigenfunctions as

$$\begin{aligned}\psi^{\text{TM}} &= \sum_n \sum_m A_{nm}^{\text{TM}} \psi_{nm}^{\text{TM}} & (\mathbf{A} = \hat{z} \psi^{\text{TM}}) \\ \psi^{\text{TE}} &= \sum_n \sum_m A_{nm}^{\text{TE}} \psi_{nm}^{\text{TE}} & (\mathbf{F} = \hat{z} \psi^{\text{TE}})\end{aligned}\quad (1)$$

the electric and magnetic fields in the guide are given by

$$\begin{aligned}\mathbf{E} &= -j\omega\mathbf{A} + \frac{1}{j\omega\mu\epsilon}\nabla\nabla\cdot\mathbf{A} - \frac{1}{\epsilon}\nabla\times\mathbf{F} = \mathbf{E}^+ + \mathbf{E}^- \\ \mathbf{H} &= -j\omega\mathbf{F} + \frac{1}{j\omega\mu\epsilon}\nabla\nabla\cdot\mathbf{F} + \frac{1}{\mu}\nabla\times\mathbf{A} = \mathbf{H}^+ + \mathbf{H}^-\end{aligned}\quad (2)$$

These can be more conveniently rewritten as

$$\begin{aligned}\mathbf{E}^+ &= \sum_n \sum_m C_{nm}^+ [\mathbf{e}_{nm} + \hat{z}e_{z_{nm}}] e^{-j\beta_{z_{nm}}z} = \sum_n \sum_m C_{nm}^+ \mathbf{E}_{nm}^+ \\ \mathbf{H}^+ &= \sum_n \sum_m C_{nm}^+ [\mathbf{h}_{nm} + \hat{z}h_{z_{nm}}] e^{-j\beta_{z_{nm}}z} = \sum_n \sum_m C_{nm}^+ \mathbf{H}_{nm}^+\end{aligned}\quad (3)$$

for the modal fields propagating in the $+z$ direction and as

$$\begin{aligned}\mathbf{E}^- &= \sum_n \sum_m C_{nm}^- [\mathbf{e}_{nm} - \hat{z}e_{z_{nm}}] e^{j\beta_{z_{nm}}z} = \sum_n \sum_m C_{nm}^- \mathbf{E}_{nm}^- \\ \mathbf{H}^- &= \sum_n \sum_m C_{nm}^- [-\mathbf{h}_{nm} + \hat{z}h_{z_{nm}}] e^{j\beta_{z_{nm}}z} = \sum_n \sum_m C_{nm}^- \mathbf{H}_{nm}^-\end{aligned}\quad (4)$$

for the modal fields propagating in the $-z$ direction. The specific form of the modal fields $(\mathbf{E}_{nm}^\pm, \mathbf{H}_{nm}^\pm)$ can be extracted from (2) once the eigenfunctions ψ^{TE} and ψ^{TM} have been determined. Note that the form of $(\mathbf{E}_{nm}^\pm, \mathbf{H}_{nm}^\pm)$ was chosen so that this pair satisfies Maxwell's equations. Thus, we can write

$$\begin{aligned}\nabla\times\mathbf{E}_{nm}^- &= -j\omega\mu\mathbf{H}_{nm}^- & \nabla\times\mathbf{E}_{nm}^+ &= -j\omega\mu\mathbf{H}_{nm}^+ \\ \nabla\times\mathbf{H}_{nm}^- &= j\omega\epsilon\mathbf{E}_{nm}^- & \nabla\times\mathbf{H}_{nm}^+ &= j\omega\epsilon\mathbf{E}_{nm}^+\end{aligned}\quad (5)$$

We are interested in finding the waveguide coefficients C_{nm} for a given electric current distribution $\mathbf{J}(\mathbf{r})$ placed within the waveguide. In the following, we present a rather standard procedure for accomplishing this.

We begin with Maxwell's equations

$$\begin{aligned}\nabla\times\mathbf{E} &= -j\omega\mu\mathbf{H} \\ \nabla\times\mathbf{H} &= +j\omega\epsilon\mathbf{E} + \mathbf{J}\end{aligned}\quad (6)$$

When these are combined with (5) we obtain that

$$\nabla\cdot(\mathbf{E}\times\mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}) = \mathbf{J}\cdot\mathbf{E}_{nm}^- \quad (7)$$

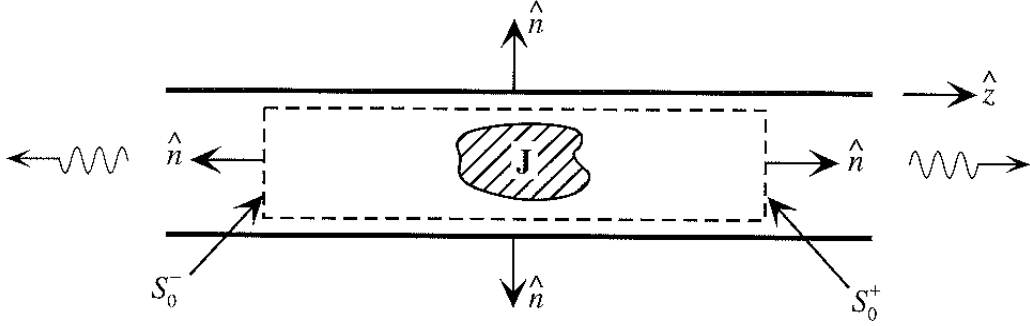
(refer to Poynting's theorem for a proof of this identity), and upon application of the divergence theorem we have

$$\iiint_V \nabla \cdot (\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}) dv = \iiint_V \mathbf{J}(\mathbf{r}) \cdot \mathbf{E}_{nm}^- dv$$

or

$$\iint_S [\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}] \cdot \hat{n} ds = \iiint_V \mathbf{J}(\mathbf{r}) \cdot \mathbf{E}_{nm}^- dv \quad (8)$$

The latter surface integral involves integration over the waveguide walls and the surfaces S_0^+ and S_0^- to the left and right of the source as illustrated in the figure below.



Since $\hat{n} \times \mathbf{E}_{nm}^-$ and $\hat{n} \times \mathbf{E}$ satisfy the boundary conditions on the waveguide's walls, it follows that

$$\iint_S [\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}] \cdot \hat{n} ds = \iint_{S_0^+ + S_0^-} [\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}] \cdot \hat{n} ds \quad (9)$$

For the last integral we have (by virtue of mode orthogonality, the infinite sums reduce to a single summand):

$$\begin{aligned} \iint_{S_0^+ + S_0^-} [\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}] \cdot ds = \\ \iint_{S_0^+} C_{nm}^+ [(\mathbf{e}_{nm} + \hat{z}e_{z_{nm}}) \times (-\mathbf{h}_{nm} + \hat{z}h_{z_{nm}}) - (\mathbf{e}_{nm} - \hat{z}e_{z_{nm}}) \times (\mathbf{h}_{nm} + \hat{z}h_{z_{nm}})] \cdot \hat{z} ds \\ + \iint_{S_0^-} C_{nm}^- (-\hat{z}) \cdot [(\mathbf{e}_{nm} - \hat{z}e_{z_{nm}}) \times (-\mathbf{h}_{nm} + \hat{z}h_{z_{nm}}) - (\mathbf{e}_{nm} - \hat{z}e_{z_{nm}}) \times (-\mathbf{h}_{nm} + \hat{z}h_{z_{nm}})] ds \end{aligned}$$

From this expansion of the fields under the integrals, it is readily seen that the integrand associated with the surface S_0^- vanishes. On making some additional cancellations in the other integral over S_0^+ , we find that

$$\iint_S [\mathbf{E} \times \mathbf{H}_{nm}^- - \mathbf{E}_{nm}^- \times \mathbf{H}] \cdot \hat{n} ds = -2C_{nm}^+ \iint_{S_0^+} (\mathbf{e}_{nm} \times \mathbf{h}_{nm}) \cdot \hat{z} dx dy \quad (10)$$

From (8), we then conclude that

$$\boxed{C_{nm}^+ = -\frac{1}{P_{nm}} \iiint_V (\mathbf{E}_{nm}^- \cdot \mathbf{J}) dv} = -\frac{1}{P_{nm}} \iiint_V (\mathbf{e}_{nm} - \hat{z}e_{z_{nm}}) \cdot \mathbf{J} e^{j\beta_{z_{nm}}z} dv \quad (11)$$

with

$$P_{nm} = 2 \iint_{S_0^+ \text{ or } S_0^-} \mathbf{e}_{nm} \times \mathbf{h}_{nm} \cdot \hat{z} dx dy$$

To find an expression for C_{nm}^- , we repeat the process with $(\mathbf{E}_{nm}^-, \mathbf{H}_{nm}^-)$ replaced by $(\mathbf{E}_{nm}^+, \mathbf{H}_{nm}^+)$. We obtain

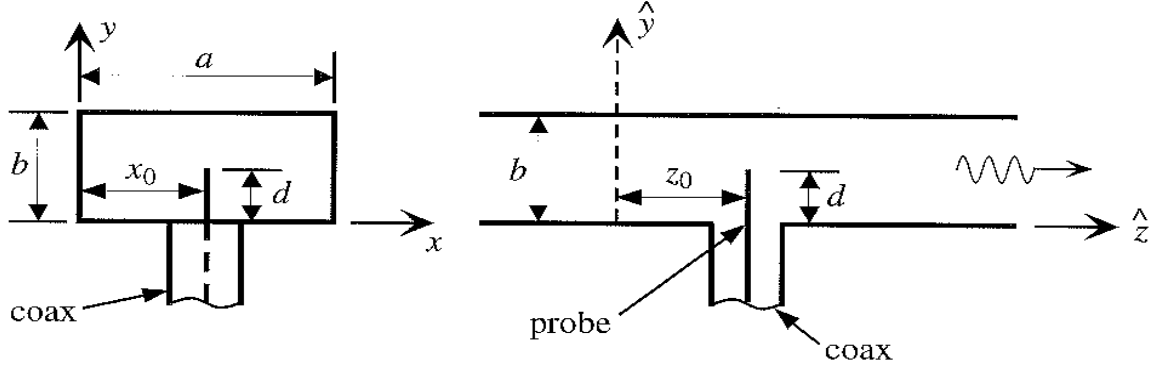
$$\boxed{C_{nm}^- = -\frac{1}{P_{nm}} \iiint_V \mathbf{E}_{nm}^+ \cdot \mathbf{J} dv}$$

When magnetic currents are present, the above expressions generalize to

$$\begin{aligned} C_{nm}^+ &= -\frac{1}{P_{nm}} \iiint_V (\mathbf{E}_{nm}^- \cdot \mathbf{J} - \mathbf{H}_{nm}^- \cdot \mathbf{M}) dV \\ C_{nm}^- &= -\frac{1}{P_{nm}} \iiint_V (\mathbf{E}_{nm}^+ \cdot \mathbf{J} - \mathbf{H}_{nm}^+ \cdot \mathbf{M}) dV \end{aligned}$$

Example

Consider a rectangular waveguide whose cross sections are shown below ($b < a$).



The fields in this guide can be represented as ($\beta = \omega\sqrt{\mu\epsilon}$, $\beta_{zmn} = \sqrt{\beta^2 - (n\pi/a)^2 - (m\pi/b)^2}$)

$$\begin{aligned} \mathbf{H}^+ &= \sum_n \sum_m A_{nm} \left\{ \frac{\beta_{zmn}}{\omega\mu\epsilon} \left[\hat{x} \frac{n\pi}{a} \sin \frac{n\pi}{a} x \cos \frac{m\pi}{b} y + \hat{y} \frac{m\pi}{b} \cos \frac{n\pi}{a} x \sin \frac{m\pi}{b} y \right] \right. \\ &\quad \left. + \hat{z} \frac{\beta^2 - \beta_{zmn}^2}{j\omega\mu\epsilon} \cos \frac{n\pi}{a} x \cos \frac{m\pi}{b} y \right\} e^{-j\beta_{zmn}z} \\ \mathbf{E}^+ &= \sum_n \sum_m \frac{A_{nm}}{\epsilon} \left[\hat{x} \frac{m\pi}{b} \cos \frac{n\pi}{a} x \sin \frac{m\pi}{b} y - \hat{y} \frac{n\pi}{a} \sin \frac{n\pi}{a} x \cos \frac{m\pi}{b} y \right] e^{-j\beta_{zmn}z} \end{aligned}$$

Consequently,

$$\begin{aligned} \mathbf{e}_{nm} &= \hat{x} \frac{m\pi}{b} \cos \frac{n\pi}{a} x \sin \frac{m\pi}{b} y - \hat{y} \frac{n\pi}{a} \sin \frac{n\pi}{a} x \cos \frac{m\pi}{b} y \\ \mathbf{h}_{nm} &= \left(\hat{x} \frac{n\pi}{a} \sin \frac{n\pi}{a} x \cos \frac{m\pi}{b} y + \hat{y} \frac{m\pi}{b} \cos \frac{n\pi}{a} x \sin \frac{m\pi}{b} y \right) \frac{\beta_{zmn}}{\omega\mu} \end{aligned}$$

and for the lowest order TE₁₀ mode, we have

$$\begin{aligned} \mathbf{e}_{10} &= -\hat{y} \frac{\pi}{a} \sin \frac{\pi}{a} x \\ \mathbf{h}_{10} &= +\hat{x} \left(\frac{\pi}{a} \sin \frac{\pi}{a} x \right) \frac{\beta_{z10}}{\omega\mu} \end{aligned}$$

By comparison with (3), $C_{nm}^+ = A_{nm}/\epsilon$.

Assuming that the probe current distribution is given by

$$I(y) = I_0 \sin \beta(d - y) \quad 0 < y < d$$

we find that

$$\begin{aligned} C_{nm}^+ &= -\frac{I_0}{P_{nm}} \int_0^d \sin[\beta(d-y)] (\mathbf{e}_{nm} \cdot \hat{\mathbf{y}}) e^{j\beta_{z_{nm}} z_0} dy \\ &= \left(\frac{n\pi}{a}\right) \frac{I_0}{P_{nm}} \sin\left(\frac{n\pi}{a} x_0\right) \int_0^d \sin[\beta(d-y)] \cos\left(\frac{m\pi}{b} y\right) dy \end{aligned}$$

For example,

$$C_{10}^+ = \left(\frac{\pi}{a}\right) \frac{I_0}{P_{10}} \sin\left(\frac{\pi}{a} x_0\right) \frac{[1 - \cos \beta_0 d]}{\beta_0}$$

with

$$P_{10} = 2 \int_0^a \int_0^b \left(\frac{\beta_{z_{10}}}{\omega\mu}\right) \left(\frac{\pi}{a}\right)^2 \sin^2 \frac{\pi x}{a} dx dy = ab \left(\frac{\beta_{z_{10}}}{\omega\mu}\right) \left(\frac{\pi}{a}\right)^2$$

mode admittance.